



# Inflow Design Flood Control System Plan

## J.C. WEADOCK GENERATING FACILITY

### BOTTOM ASH POND INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

Essexville, Michigan

Pursuant to 40 CFR 257.82

**Submitted To:** Consumers Energy Company  
1945 W. Parnall Road  
Jackson, Michigan 49201

**Submitted By:** Golder Associates Inc.  
15851 South US 27, Suite 50  
Lansing, Michigan 48906

October 2016

1655164





**CERTIFICATION**

**Professional Engineer Certification Statement [40 CFR 257.82(c)]**

I hereby certify that, having reviewed the attached documentation and being familiar with the provisions of Title 40 of the Code of Federal Regulations Section 257.82 (40 CFR Part 257.82), I attest that this Inflow Design Flood Control System Plan is accurate and has been prepared in accordance with good engineering practices, including the consideration of applicable industry standards, and with the requirements of 40 CFR Part 257.82.

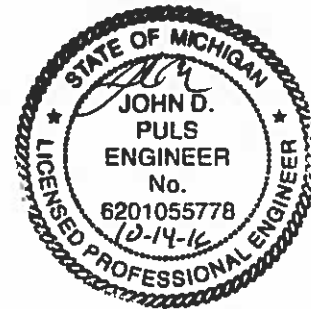
Golder Associates Inc.

  
\_\_\_\_\_  
Signature

October 14, 2016  
\_\_\_\_\_  
Date of Report Certification

John D. Puls, PE  
\_\_\_\_\_  
Name

6201055787  
\_\_\_\_\_  
Professional Engineer Certification Number





## Table of Contents

CERTIFICATION..... C-1  
Professional Engineer Certification Statement [40 CFR 257.82(c)]..... C-1

1.0 INTRODUCTION..... 1  
1.1 Background ..... 1  
1.2 Purpose ..... 1

2.0 FLOOD CONTROL SYSTEM ..... 2  
2.1 External Floodwater Protection ..... 2  
2.2 Internal Flood Control..... 2

3.0 PLAN REVISION AND RECORDKEEPING ..... 4

4.0 REFERENCES..... 5

### List of Tables

Table 2.2.1 Discharge Structure Summary  
Table 2.2.2 Storm Flow Data

### List of Figures

Figure 1 Site Location Map  
Figure 2 Site Plan

### List of Appendices

Appendix A FEMA Flood Elevation and Lake Huron Normal Elevation  
Appendix B Rainfall Data  
Appendix C Hydrologic and Hydraulic Model Output



## 1.0 INTRODUCTION

### 1.1 Background

J.C. Weadock Generating Facility (JC Weadock) is a coal-fired power generation facility located near Essexville, Michigan as presented on Figure 1 – Site Location Map. JC Weadock formerly operated two coal-burning baseload units but ceased electrical generation on April 15, 2016. Prior to stopping electrical generation, bottom ash was sluiced from JC Weadock to the Bottom Ash Pond, Areas 1 and 2. Stored bottom ash was mechanically removed from the pond as needed to maintain storage capacity. The Bottom Ash Pond discharged water via two steel outflow pipes. The pipes discharge to an internal channel network and then to the permitted National Pollutant Discharge Elimination System (NPDES) outfall as provided on Figure 2 - Site Plan. Currently, JC Weadock is being decommissioned. The Bottom Ash Pond is no longer receiving coal combustion residual (CCR) from an active power generating plant. The Bottom Ash Pond is anticipated to accept negligible amounts of CCR contact wash water and other low-volume miscellaneous wastewaters. It is anticipated that the Bottom Ash Pond's final receipt of waste will occur on or before October 1, 2018; and resulting subsequent closure activities will commence within regulated timeframes.

### 1.2 Purpose

The purpose of the Inflow Design Flood Control System Plan (Plan) is to provide a basis for the certification required by 40 CFR 257.82 (Hydrologic and Hydraulic Capacity Requirements for CCR Surface Impoundments). The Bottom Ash Pond has been rated a low hazard potential as determined under 40 CFR 257.73(a)(2). 40 CFR 257.82(a) requires the owner or operator of the low hazard potential CCR surface impoundment to design, construct, operate, and maintain an inflow design flood control system as follows:

- Adequately manage the flow into the CCR unit during and following the peak discharge of the inflow of the 100-year flood event
- Adequately manage the flow from the CCR unit to collect and control the peak discharge resulting from the 100-year flood event
- Handle discharge from the CCR unit in accordance with the surface water requirements under 40 CFR 257.3-3



## 2.0 FLOOD CONTROL SYSTEM

To meet the requirements of 40 CFR 257.82(a), the flood control system must provide flood protection to the CCR unit during the inflow design flood (100-year event) for two cases: 1) floodwater from outside the unit from Saginaw River and from Saginaw Bay, and 2) controlling internal water levels within the unit.

### 2.1 External Floodwater Protection

The Bottom Ash Pond is surrounded by a perimeter berm that provides external flood water protection. Based on borings completed in 2016, the berm is generally constructed of sand and CCR.

A publicly available 100-year flood elevation for Saginaw Bay has been determined by Federal Emergency Management Agency (FEMA). Based on FEMA Firm Map Numbers 26017C0238E and 26017C0239E, both Saginaw River and Saginaw Bay have 100-year flood elevations of 585.00 feet (NAVD88) as provided in Appendix A – FEMA Flood Elevation and Lake Huron Normal Elevation. The lowest elevation along the perimeter berm of Bottom Ash Pond Area 1 is 598.96 feet (NAVD88) and Bottom Ash Pond Area 2 is 596.68 feet (NAVD88), which allows for 13.96 and 11.68 feet of freeboard during the 100-year flood event, respectively. Therefore, the Saginaw Bay and Saginaw River should not be an inflow source to the Bottom Ash Pond.

### 2.2 Internal Flood Control

The only inflow will be precipitation directly falling on the Bottom Ash Pond and surrounding drainage areas from a 100-year 24-hour storm event of 5.99 inches, as provided in Appendix B - Rainfall Data. There are two discharge structures in the perimeter berm: two 24-inch steel pipes. Table 2.2.1 below provides a summary of the outflow structures as surveyed in May 2016.

**Table 2.2.1 - Discharge Structure Summary**

Discharge Structure	Type	Size (Inches)	Length (Feet)	Upstream Invert (NAVD88)	Downstream Invert (NAVD88)	Slope (%)
Bottom Ash Pond Area 1 Culvert	Steel	24	40	596.01	595.20	2.02
Bottom Ash Pond Area 2 Culvert	Steel	24	121	590.36	590.07	0.24

Table 2.2.2 below provides a storm flow summary that indicates that Bottom Ash Pond Area 1 is contained with 2.1 feet of freeboard, a peak discharge rate of 0.00 cubic feet per second (cfs), and outflow volume of 0.00 acre-feet during the design storm event (100-year 24-hour). Bottom Ash Pond Area 2 is contained with 4.15 feet of freeboard, a peak discharge rate of 9.30 cfs, and outflow volume of 4.67 acre-feet during the design storm event (100-year 24-hour). The modeled results indicate that:



- The inflow design flood control system adequately manages flow from the CCR unit to collect and control the peak discharge resulting from the inflow design flood (100-year 24-hour storm event)

The hydrologic and hydraulic model output is provided in Appendix C - Hydrologic and Hydraulic Model Output. It should be noted that the pond elevations presented in Table 2.2.2 were used to assess the maximum storage pool loading condition pursuant to 40 CFR 257.73(e)(1)(i).

**Table 2.2.2 – Storm Flow Data**

<b>Area</b>	<b>Perimeter Berm Elevation (NAVD88)</b>	<b>Pond Elevation 100-year, 24-hour (NAVD88)</b>	<b>Peak Outflow (cfs)</b>	<b>Volume of Outflow (acre-feet)</b>
Bottom Ash Pond Area 1	598.96	596.86	0.00	0.00
Bottom Ash Pond Area 2	596.68	592.53	9.30	4.67



### 3.0 PLAN REVISION AND RECORDKEEPING

Per 40 CFR 257.82(c)(2); “The owner or operator of the CCR unit may amend the written inflow design flood control system plan at any time provided the revised plan is placed in the facility's operating record as required by Section 257.105(g)(4). The owner or operator must amend the written inflow design flood control system plan whenever there is a change in conditions that would substantially affect the written plan in effect.”

Per 40 CFR 257.82(c)(4); “The owner or operator must prepare periodic inflow design flood control system plans required by paragraph (c)(1) of this section every five years. The date of completing the initial plan is the basis for establishing the deadline to complete the first periodic plan. The owner or operator may complete any required plan prior to the required deadline provided the owner or operator places the completed plan into the facility's operating record within a reasonable amount of time. In all cases, the deadline for completing a subsequent plan is based on the date of completing the previous plan. For purposes of this paragraph (c)(4), the owner or operator has completed an inflow design flood control system plan when the plan has been placed in the facility's operating record as required by Section 257.105(g)(4).”



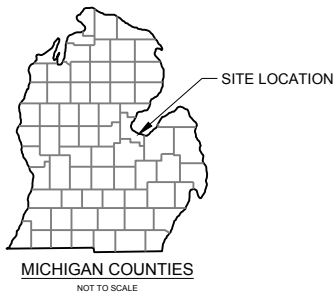
## 4.0 REFERENCES

FEMA (Federal Emergency Management Agency). 2010. Flood Insurance Study, Bay County, Michigan. Effective September 17, 2010. Flood Insurance Study Number 26017CV000A.

USEPA (US Environmental Protection Agency). 2015. Disposal of Coal Combustion Residuals from Electric Utilities; Final Rule. 40 CFR Part 257. Effective Date October 19, 2015.



## FIGURES



**REFERENCE(S)**  
 BASE MAP TAKEN FROM USGS 7.5 MINUTE QUADRANGLE  
 BAY CITY NE, MICHIGAN  
 DATED 2014



CLIENT  
**CONSUMERS ENERGY COMPANY**  
 2742 NORTH WEADOCK HIGHWAY  
 ESSEXVILLE, MI. 48732

PROJECT  
**J.C. WEADOCK**  
**BOTTOM ASH POND**

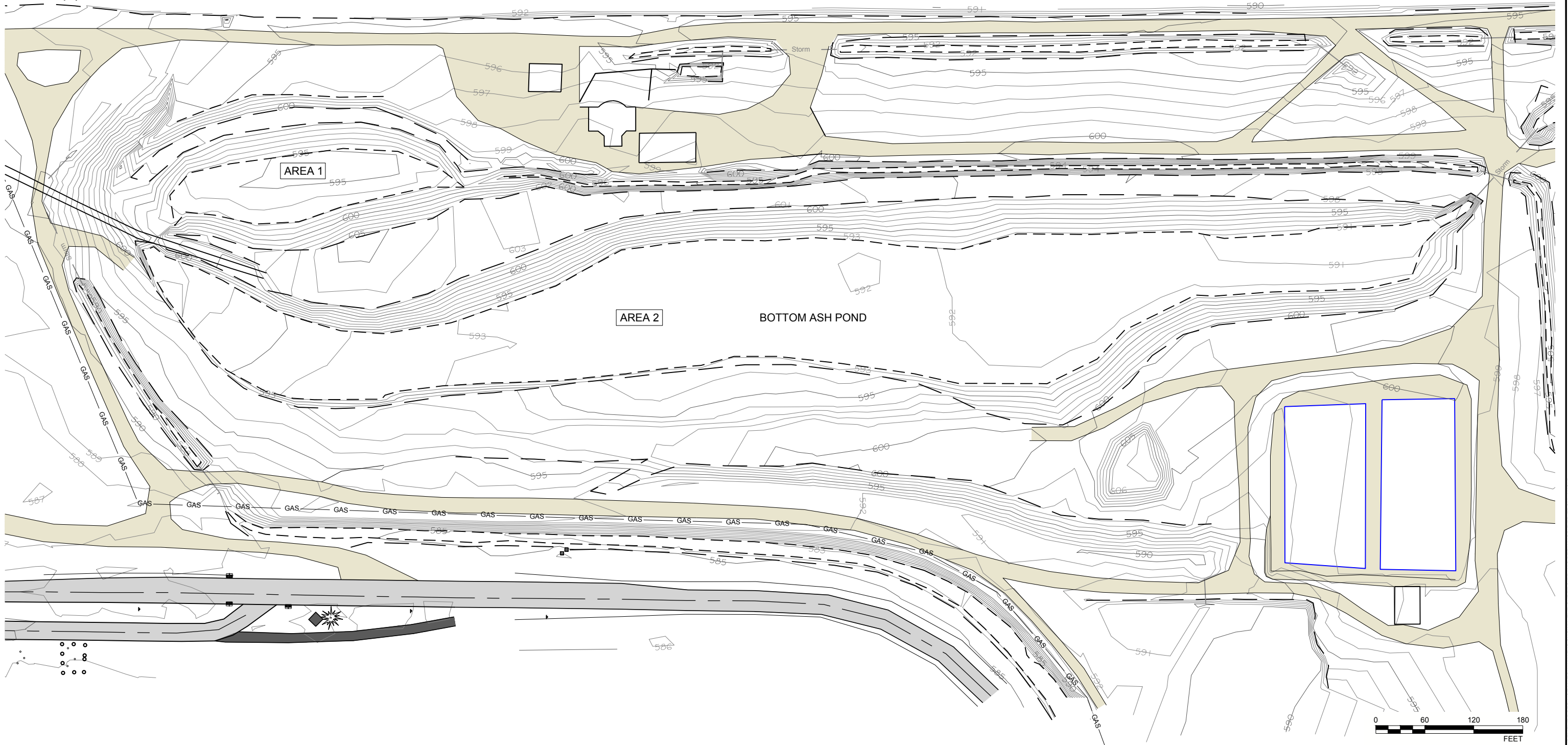
CONSULTANT	YYYY-MM-DD	2016-08-22
	DESIGNED	MAL
	PREPARED	MAL
	REVIEWED	JRP
	APPROVED	MAB

TITLE  
**SITE LOCATION MAP**

PROJECT NO.  
 1655164

REV.  
 0

FIGURE  
 1



Path: \\arcment\local\Share\Work for Other Offices\Kam & Weadock\Civil\_3D\1 File Name: 1655164\_2016-09-09 Survey.dwg

CLIENT  
 CONSUMERS ENERGY COMPANY  
 2742 NORTH WEADOCK HIGHWAY  
 ESSEXVILLE, MI. 48732

CONSULTANT



YYYY-MM-DD	2016-09-09
DESIGNED	MAL
PREPARED	MAL
REVIEWED	JRP
APPROVED	JDP

PROJECT  
 J.C. WEADOCK BOTTOM ASH POND

TITLE  
**SITE PLAN**

PROJECT NO.  
 1655164

REV.  
 ---

FIGURE  
**2**

1 in. IF THIS MEASUREMENT DOES NOT MATCH WHAT IS SHOWN, THE SHEET SIZE HAS BEEN MODIFIED FROM ANSI B

**APPENDIX A**  
**FEMA FLOOD ELEVATION AND LAKE HURON NORMAL ELEVATION**



**NOTES TO USERS**

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations (BFEs)** and/or **Floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Damwater Elevations tables contained within the Flood Insurance Study (FIS) Report that accompanies the FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS Report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

**Coastal Base Flood Elevations** shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Damwater Elevations table in the Flood Insurance Study Report for this jurisdiction. Elevations shown in the Summary of Damwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study Report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study Report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 16. The horizontal datum was NAD 83, GRS 1980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of the FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <http://www.ngs.noaa.gov> or contact the National Geodetic Survey at the following address:

NGS Information Services  
NOAA, NNGS12  
National Geodetic Survey  
SSMC-3, #9202  
1315 East-West Highway  
Silver Spring, Maryland 20910-3282  
(301) 713-3242

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242, or visit its website at <http://www.ngs.noaa.gov>.

**Base Map** information shown on this FIRM was provided in digital format by Bay County, Michigan. This information was photogrammetrically compiled at a scale of 1:200 from aerial photography dated 2005.

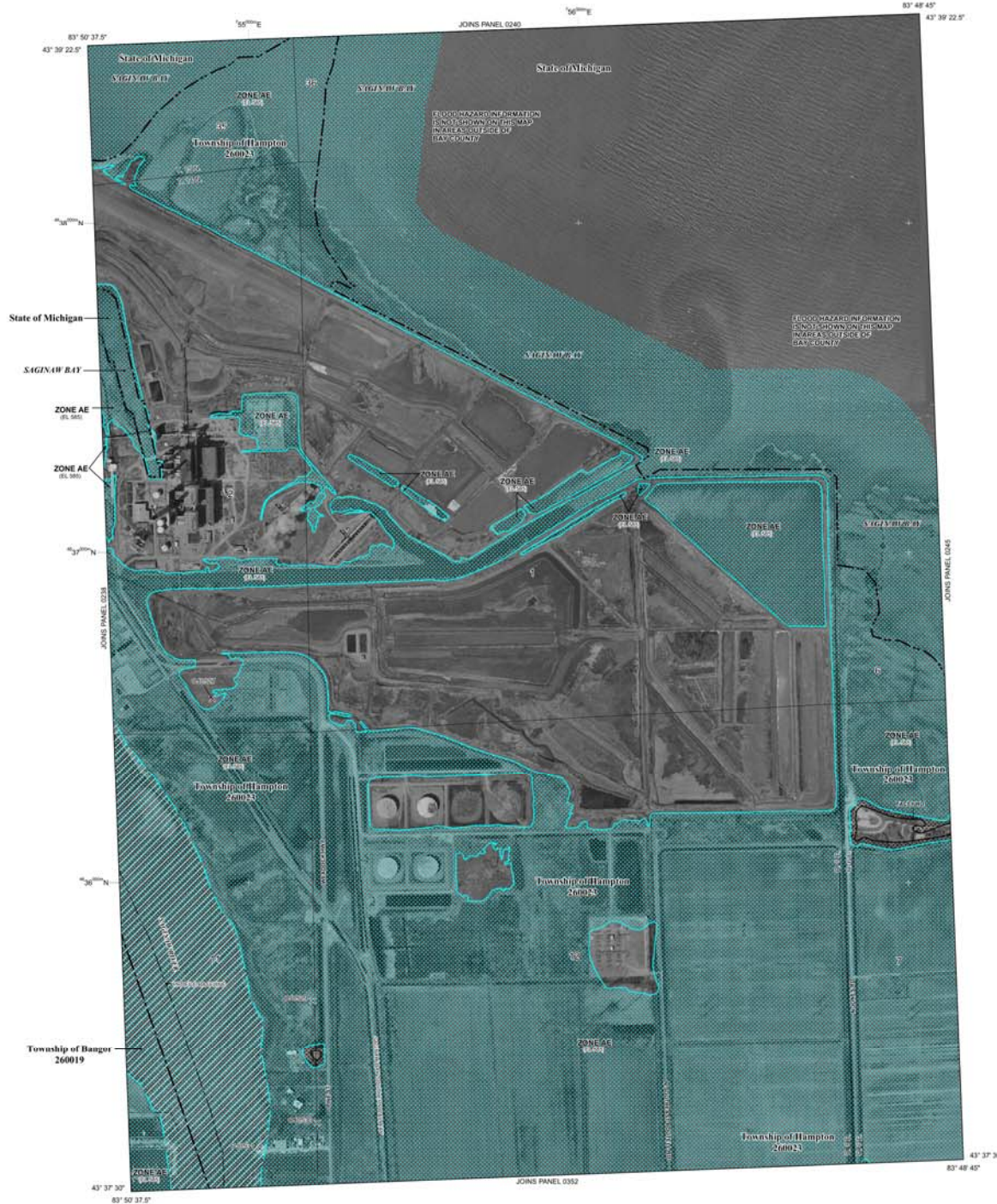
The **profile baselines** depicted on this map represent the hydraulic modeling baselines that match the flood profiles in the FIS report. As a result of improved topographic data, the **profile baseline**, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

**Corporate limits** shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the **FEMA Map Service Center** at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <http://www.fema.gov>.

If you have **questions about this map** or questions concerning the National Flood Insurance Program in general, please call 1-877-FEMA-MAP (1-877-358-2627) or visit the FEMA website at <http://www.fema.gov/business/firm>.



**LEGEND**

**SPECIAL FLOOD HAZARD AREAS (SFHAs) SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**

The 1% annual chance flood (100-year flood), also known as the "base flood," is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zone A, AE, AH, AO, AR, ARB, and VE. The Base Flood Elevation is the water surface elevation of the 1% annual chance flood.

**ZONE A**  
No Base Flood Elevations determined.

**ZONE AE**  
Base Flood Elevations determined.

**ZONE AH**  
Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); Base Flood Elevations determined.

**ZONE AO**  
Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined; Area of shallow flooding; velocities also determined.

**ZONE AR**  
Special Flood Hazard Areas formerly protected from the 1% annual chance flood by a flood control system that was subsequently destroyed. Zone AR indicates that the former flood control system is being retained to provide protection from the 1% annual chance or greater flood.

**ZONE ARB**  
Area to be protected from the 1% annual chance flood by a flood control protection system under construction; no Base Flood Elevations determined.

**ZONE V**  
Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.

**ZONE VE**  
Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

**FLOODWAY AREAS IN ZONE AE**

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachments so that the 1% annual chance flood can be carried without substantial increases in flood heights.

**OTHER FLOOD AREAS**

**ZONE K**  
Areas of 0.2% annual chance flood, areas of 1% annual chance flood with average depths of less than 1 foot or with discharge areas less than 1 square mile, and areas protected by levees from the 1% annual chance flood.

**OTHER AREAS**

**ZONE D**  
Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible.

**COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS**

**OTHERWISE PROTECTED AREAS (OPAs)**

CBRS areas and OPAs are normally marked within or adjacent to Special Flood Hazard Areas.

1% Annual Chance Floodplain Boundary  
0.2% Annual Chance Floodplain Boundary  
Floodway boundary  
Zone D boundary  
CBRS and OPA boundary  
Boundary defining Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities  
Base Flood Elevation line and value, elevation in feet  
Base Flood Elevation value where uniform within zone; elevation in feet

Referenced to the North American Vertical Datum of 1988

○ Cross section line  
○ Transient line  
47° 52' 00" 83° 12' 12" Geographic coordinates referenced to the North American Datum of 1983 (NAD 83) (NAD 83) (NAD 83) (NAD 83)  
1000-meter Universal Transverse Mercator grid values, zone 16E  
X Bench mark (see explanation in Notes to Users section of this FIS report)  
\* BFE  
Bench Mark

**MAP REPOSITORIES**  
Refer to Map Repository List on Map Index

**EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP**  
June 16, 2008

**EFFECTIVE DATE(S) OF REVISION(S) TO THIS PANEL**  
September 17, 2010 - to add Special Flood Hazard Areas and update and read names, to change Special Flood Hazard Areas, to update corporate limits and map format, to incorporate previously issued Letters of Map Change, and to effect additional topographic information.

For community map revision history prior to complete mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction.

To determine if flood insurance is available in the community, contact your insurance agent or call the National Flood Insurance Program at 1-800-485-6020.

**MAP SCALE 1" = 500'**

250 0 500 1000  
0 0 150 300  
FEET  
METERS

**NFIP**

**PANEL 0239E**

**FIRM**

**FLOOD INSURANCE RATE MAP**

**BAY COUNTY, MICHIGAN**

**ALL JURISDICTIONS**

**PANEL 230 OF 450**  
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

COUNTY	TOWNSHIP	NUMBER	PANEL	SUFFIX
BAY COUNTY	HAMPTON TOWNSHIP	26019	0239	E
		26023	0239	E

Notice to User: The **Map Number** shown below should be used when placing map orders. The **Community Number** shown above should be used on insurance applications for the subject community.

**MAP NUMBER 26017C0239E**

**MAP REVISED SEPTEMBER 17, 2010**

Federal Emergency Management Agency

**APPENDIX B  
RAINFALL DATA**



**NOAA Atlas 14, Volume 8, Version 2**  
**Location name: Essexville, Michigan, US\***  
**Latitude: 43.6433°, Longitude: -83.8376°**  
**Elevation: 585 ft\***  
 \* source: Google Maps



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffrey Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

**PF tabular**

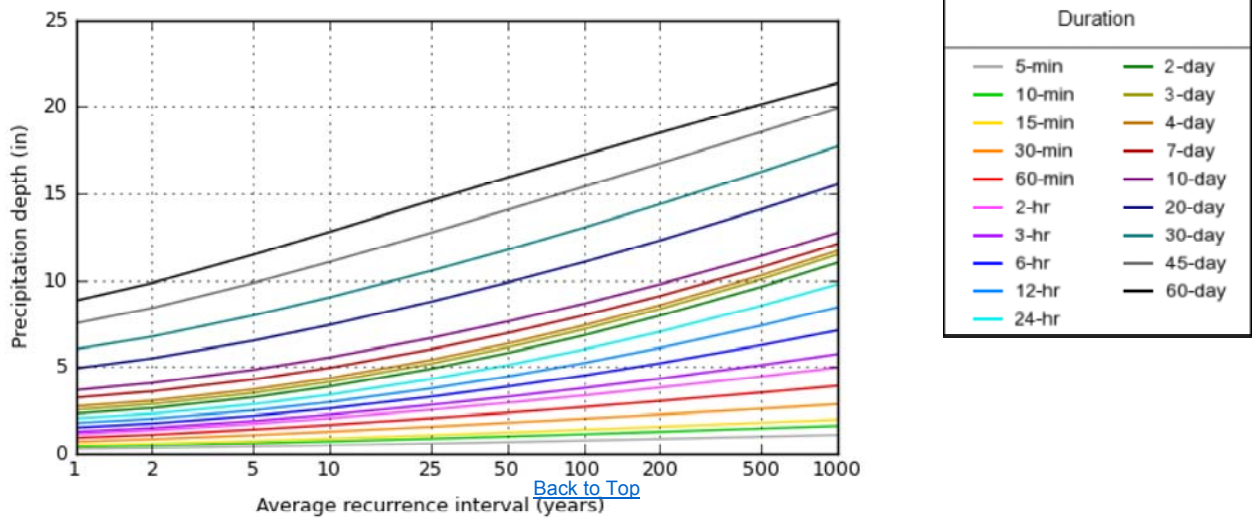
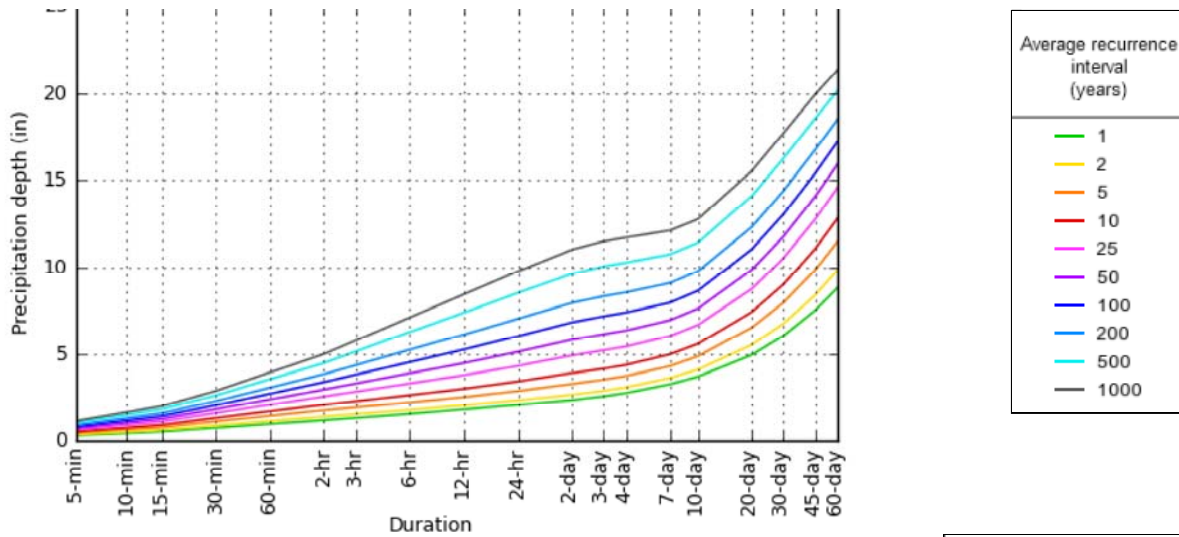
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.281 (0.221-0.364)	0.333 (0.262-0.432)	0.421 (0.331-0.548)	0.497 (0.388-0.651)	0.606 (0.458-0.829)	0.693 (0.510-0.963)	0.783 (0.556-1.12)	0.877 (0.595-1.30)	1.01 (0.655-1.54)	1.11 (0.700-1.72)
10-min	0.411 (0.324-0.533)	0.487 (0.384-0.632)	0.617 (0.484-0.803)	0.728 (0.568-0.953)	0.887 (0.670-1.21)	1.02 (0.747-1.41)	1.15 (0.814-1.64)	1.28 (0.872-1.90)	1.47 (0.959-2.25)	1.62 (1.03-2.52)
15-min	0.501 (0.396-0.649)	0.594 (0.469-0.771)	0.752 (0.591-0.979)	0.888 (0.693-1.16)	1.08 (0.817-1.48)	1.24 (0.911-1.72)	1.40 (0.992-2.00)	1.57 (1.06-2.32)	1.80 (1.17-2.75)	1.98 (1.25-3.07)
30-min	0.722 (0.570-0.936)	0.859 (0.678-1.12)	1.09 (0.856-1.42)	1.29 (1.01-1.69)	1.57 (1.19-2.15)	1.80 (1.32-2.49)	2.03 (1.44-2.90)	2.27 (1.54-3.35)	2.60 (1.69-3.97)	2.86 (1.81-4.44)
60-min	0.940 (0.742-1.22)	1.11 (0.877-1.44)	1.41 (1.11-1.84)	1.67 (1.31-2.19)	2.05 (1.56-2.82)	2.37 (1.74-3.30)	2.69 (1.91-3.87)	3.04 (2.07-4.51)	3.52 (2.30-5.40)	3.91 (2.47-6.07)
2-hr	1.16 (0.925-1.48)	1.36 (1.09-1.75)	1.73 (1.38-2.22)	2.05 (1.62-2.65)	2.54 (1.95-3.45)	2.94 (2.19-4.05)	3.36 (2.42-4.78)	3.81 (2.62-5.60)	4.45 (2.94-6.76)	4.96 (3.17-7.63)
3-hr	1.29 (1.04-1.63)	1.51 (1.21-1.91)	1.90 (1.52-2.42)	2.26 (1.80-2.90)	2.81 (2.18-3.81)	3.28 (2.47-4.51)	3.78 (2.74-5.36)	4.33 (3.00-6.33)	5.10 (3.39-7.72)	5.73 (3.69-8.77)
6-hr	1.52 (1.24-1.90)	1.75 (1.43-2.20)	2.19 (1.78-2.75)	2.61 (2.11-3.30)	3.28 (2.59-4.42)	3.86 (2.95-5.27)	4.50 (3.31-6.33)	5.21 (3.66-7.57)	6.24 (4.20-9.37)	7.09 (4.61-10.7)
12-hr	1.78 (1.47-2.20)	2.02 (1.67-2.50)	2.50 (2.06-3.10)	2.98 (2.43-3.71)	3.75 (3.01-5.02)	4.44 (3.45-6.02)	5.22 (3.89-7.28)	6.09 (4.34-8.78)	7.36 (5.02-11.0)	8.43 (5.54-12.6)
24-hr	2.05 (1.71-2.49)	2.31 (1.93-2.81)	2.85 (2.37-3.48)	3.40 (2.81-4.17)	4.29 (3.49-5.67)	5.09 (4.00-6.81)	5.99 (4.53-8.27)	7.01 (5.05-10.0)	8.51 (5.87-12.6)	9.77 (6.49-14.5)
2-day	2.33 (1.97-2.78)	2.64 (2.23-3.16)	3.25 (2.74-3.91)	3.87 (3.25-4.69)	4.88 (4.02-6.37)	5.79 (4.61-7.64)	6.80 (5.20-9.26)	7.94 (5.79-11.2)	9.62 (6.70-14.0)	11.0 (7.39-16.2)
3-day	2.55 (2.17-3.02)	2.86 (2.44-3.40)	3.50 (2.97-4.17)	4.14 (3.49-4.96)	5.18 (4.29-6.69)	6.11 (4.90-7.99)	7.15 (5.50-9.66)	8.32 (6.11-11.7)	10.1 (7.05-14.6)	11.5 (7.76-16.8)
4-day	2.74 (2.35-3.23)	3.06 (2.63-3.61)	3.70 (3.16-4.39)	4.35 (3.69-5.18)	5.39 (4.49-6.91)	6.33 (5.10-8.22)	7.37 (5.70-9.90)	8.55 (6.30-11.9)	10.3 (7.24-14.8)	11.7 (7.95-17.0)
7-day	3.23 (2.81-3.76)	3.59 (3.11-4.19)	4.28 (3.70-5.01)	4.94 (4.24-5.82)	6.00 (5.03-7.55)	6.93 (5.62-8.86)	7.95 (6.20-10.5)	9.09 (6.75-12.5)	10.7 (7.63-15.3)	12.1 (8.29-17.4)
10-day	3.67 (3.20-4.23)	4.07 (3.56-4.71)	4.83 (4.20-5.60)	5.54 (4.79-6.47)	6.64 (5.59-8.26)	7.59 (6.19-9.60)	8.63 (6.76-11.3)	9.77 (7.29-13.3)	11.4 (8.14-16.1)	12.8 (8.78-18.2)
20-day	4.91 (4.35-5.58)	5.49 (4.86-6.25)	6.50 (5.73-7.43)	7.40 (6.48-8.52)	8.75 (7.42-10.6)	9.86 (8.12-12.2)	11.0 (8.73-14.2)	12.3 (9.27-16.5)	14.1 (10.1-19.6)	15.5 (10.8-22.0)
30-day	6.02 (5.37-6.78)	6.73 (6.01-7.59)	7.95 (7.07-9.00)	9.01 (7.95-10.3)	10.5 (8.97-12.6)	11.8 (9.75-14.4)	13.0 (10.4-16.6)	14.4 (10.9-19.0)	16.2 (11.8-22.4)	17.7 (12.4-24.9)
45-day	7.49 (6.75-8.36)	8.38 (7.54-9.36)	9.84 (8.82-11.0)	11.1 (9.84-12.5)	12.7 (10.9-15.1)	14.1 (11.7-17.0)	15.4 (12.3-19.3)	16.7 (12.7-21.9)	18.5 (13.5-25.3)	19.9 (14.0-27.8)
60-day	8.81 (7.99-9.77)	9.84 (8.90-10.9)	11.5 (10.3-12.8)	12.8 (11.5-14.4)	14.6 (12.5-17.0)	15.9 (13.3-19.0)	17.2 (13.8-21.4)	18.5 (14.1-24.0)	20.1 (14.7-27.2)	21.3 (15.1-29.7)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

**PF graphical**





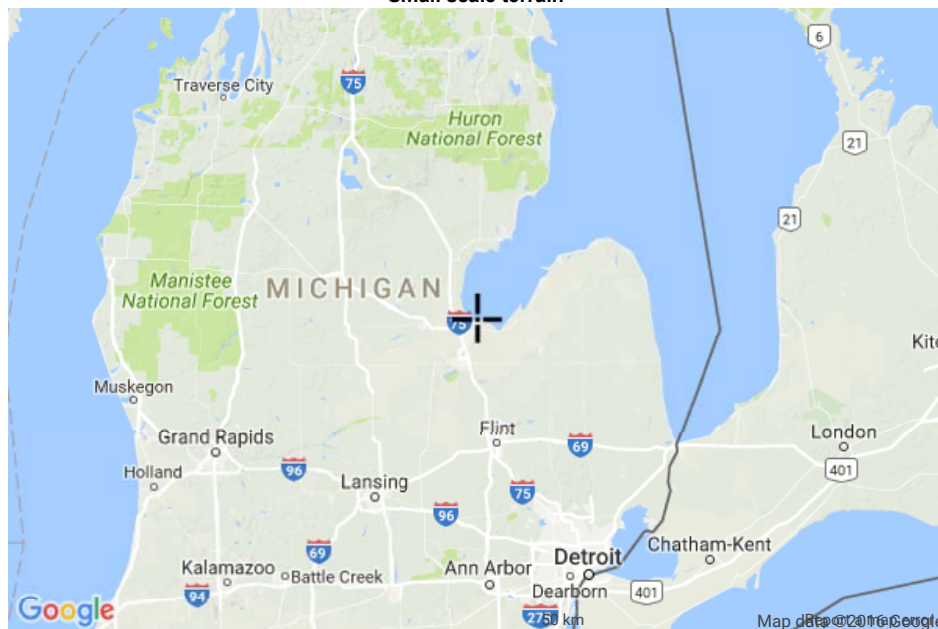
[Back to Top](#)

### Maps & aeriels

NOAA Atlas 14, Volume 8, Version 2

Created (GMT): Thu Aug 18 12:43:50 2016

#### Small scale terrain





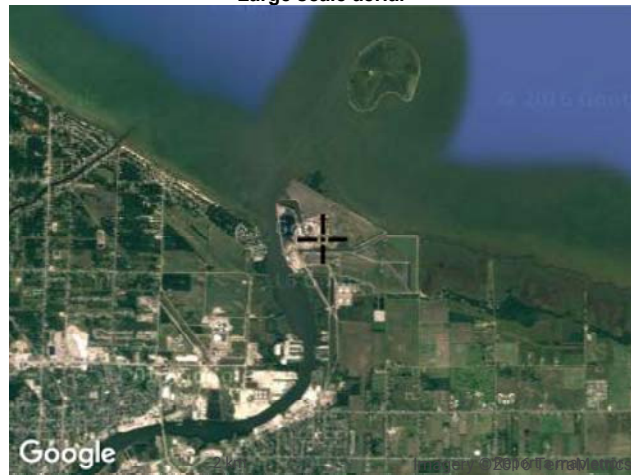
**Large scale terrain**



**Large scale map**



**Large scale aerial**



[Back to Top](#)

---

[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910

Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

[Disclaimer](#)

**APPENDIX C**  
**HYDROLOGIC AND HYDRAULIC MODEL OUTPUT**

## Project Description

File Name ..... Weadock\_2.SPF

## Project Options

Flow Units ..... CFS  
 Elevation Type ..... Elevation  
 Hydrology Method ..... SCS TR-55  
 Time of Concentration (TOC) Method ..... SCS TR-55  
 Link Routing Method ..... Hydrodynamic  
 Enable Overflow Ponding at Nodes ..... YES  
 Skip Steady State Analysis Time Periods ..... NO

## Analysis Options

Start Analysis On ..... Aug 04, 2016 00:00:00  
 End Analysis On ..... Aug 06, 2016 00:00:00  
 Start Reporting On ..... Aug 04, 2016 00:00:00  
 Antecedent Dry Days ..... 0 days  
 Runoff (Dry Weather) Time Step ..... 0 01:00:00 days hh:mm:ss  
 Runoff (Wet Weather) Time Step ..... 0 00:05:00 days hh:mm:ss  
 Reporting Time Step ..... 0 00:05:00 days hh:mm:ss  
 Routing Time Step ..... 30 seconds

## Number of Elements

	Qty
Rain Gages .....	1
Subbasins.....	2
Nodes.....	5
<i>Junctions</i> .....	1
<i>Outfalls</i> .....	2
<i>Flow Diversions</i> .....	0
<i>Inlets</i> .....	0
<i>Storage Nodes</i> .....	2
Links.....	3
<i>Channels</i> .....	1
<i>Pipes</i> .....	2
<i>Pumps</i> .....	0
<i>Orifices</i> .....	0
<i>Weirs</i> .....	0
<i>Outlets</i> .....	0
Pollutants .....	0
Land Uses .....	0

## Rainfall Details

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County	Return Period (years)	Rainfall Depth (inches)	Rainfall Distribution
1	Rain Gage-01	Time Series	TS-100	Cumulative	inches	Michigan	None	100	5.99	SCS Type II 24-hr

## Subbasin Summary

SN	Subbasin ID	Area	Weighted Curve Number	Total Rainfall	Total Runoff	Total Runoff Volume	Peak Runoff	Time of Concentration
		(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
1	Sub-01	9.78	98.00	5.99	5.75	56.25	76.90	0 00:05:00
2	Sub-02	1.34	98.00	5.99	5.75	7.71	10.52	0 00:05:00

## Node Summary

SN	Element ID	Element Type	Invert Elevation (ft)	Ground/Rim (Max) Elevation (ft)	Initial Water Elevation (ft)	Surcharge Elevation (ft)	Ponded Area (ft <sup>2</sup> )	Peak Inflow (cfs)	Max HGL Elevation Attained (ft)	Max Surcharge Depth Attained (ft)	Min Freeboard Attained (ft)	Time of Peak Flooding Occurrence (days hh:mm)	Total Flooded Volume (ac-in)	Total Time Flooded (min)
1	Jun-02	Junction	596.01	6.00	0.00	0.00	0.00	0.00	596.01	0.00	3.00	0 00:00	0.00	0.00
2	Out-01	Outfall	590.07					9.30	591.16					
3	Out-02	Outfall	595.20					0.00	595.20					
4	PondArea1	Storage Node	595.00	598.96	595.00		0.00	10.52	596.86				0.00	0.00
5	PondArea2	Storage Node	590.00	596.68	590.36		0.00	76.88	592.53				0.00	0.00

## Link Summary

SN Element ID	Element Type	From (Inlet) Node	To (Outlet) Node	Length (ft)	Inlet Invert Elevation (ft)	Outlet Invert Elevation (ft)	Average Slope (%)	Diameter or Height (ft)	Manning's Roughness	Peak Flow (cfs)	Design Flow Capacity (cfs)	Peak Flow/ Design Flow Ratio	Peak Flow Velocity (ft/sec)	Peak Flow Depth (ft)	Peak Flow Depth/ Total Depth Ratio	Total Time Reported (min)	Reported Condition	
1	PondArea1Culvert	Pipe	Jun-02	Out-02	40.00	596.01	595.20	2.0200	2.000	0.0250	0.00	16.74	0.00	0.00	0.00	0.00	0.00	Calculated
2	PondArea2Culvert	Pipe	PondArea2	Out-01	121.00	590.36	590.07	0.2400	2.000	0.0240	9.30	6.00	1.55	3.57	1.54	0.77	0.00	> CAPACITY
3	PondArea1Channel	Channel	PondArea1	Jun-02	1241.00	598.00	596.01	0.1600	3.000	0.0320	0.00	69.96	0.00	0.00	0.00	0.00	0.00	

# Subbasin Hydrology

## Subbasin : Sub-01

### Input Data

Area (ac) ..... 9.78  
 Weighted Curve Number ..... 98.00  
 Rain Gage ID ..... Rain Gage-01

### Composite Curve Number

Soil/Surface Description	Area (acres)	Soil Group	Curve Number
-	9.78	-	98.00
Composite Area & Weighted CN	9.78		98.00

### Time of Concentration

TOC Method : SCS TR-55

Sheet Flow Equation :

$$T_c = (0.007 * ((n * L_f)^{0.8}) / ((P^{0.5}) * (S_f^{0.4})))$$

Where :

Tc = Time of Concentration (hr)  
 n = Manning's roughness  
 Lf = Flow Length (ft)  
 P = 2 yr, 24 hr Rainfall (inches)  
 Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation :

V = 16.1345 \* (Sf<sup>0.5</sup>) (unpaved surface)  
 V = 20.3282 \* (Sf<sup>0.5</sup>) (paved surface)  
 V = 15.0 \* (Sf<sup>0.5</sup>) (grassed waterway surface)  
 V = 10.0 \* (Sf<sup>0.5</sup>) (nearly bare & untilled surface)  
 V = 9.0 \* (Sf<sup>0.5</sup>) (cultivated straight rows surface)  
 V = 7.0 \* (Sf<sup>0.5</sup>) (short grass pasture surface)  
 V = 5.0 \* (Sf<sup>0.5</sup>) (woodland surface)  
 V = 2.5 \* (Sf<sup>0.5</sup>) (forest w/heavy litter surface)  
 Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)  
 Lf = Flow Length (ft)  
 V = Velocity (ft/sec)  
 Sf = Slope (ft/ft)

Channel Flow Equation :

$$V = (1.49 * (R^{2/3}) * (S_f^{0.5})) / n$$

R = Aq / Wp  
 Tc = (Lf / V) / (3600 sec/hr)

Where :

Tc = Time of Concentration (hr)  
 Lf = Flow Length (ft)  
 R = Hydraulic Radius (ft)  
 Aq = Flow Area (ft<sup>2</sup>)  
 Wp = Wetted Perimeter (ft)  
 V = Velocity (ft/sec)  
 Sf = Slope (ft/ft)  
 n = Manning's roughness

User-Defined TOC override (minutes): 5

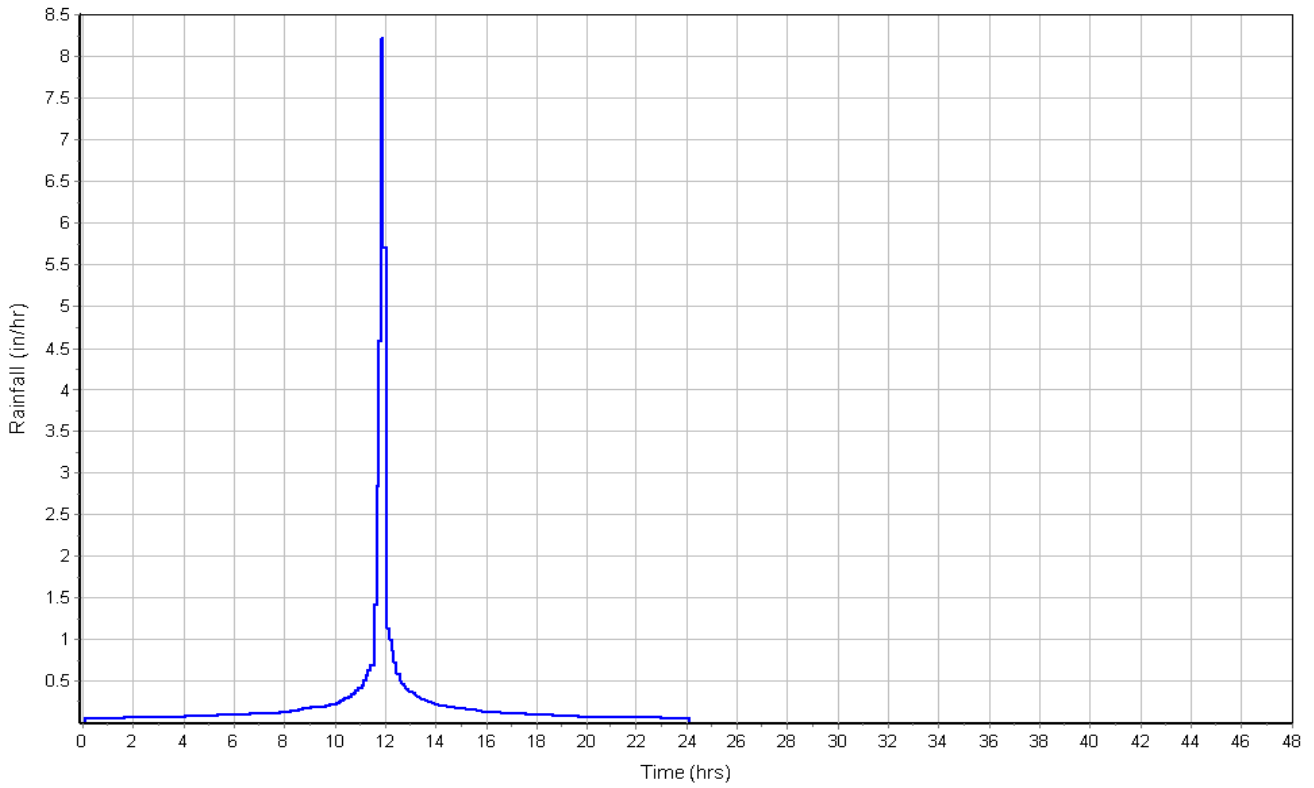
### Subbasin Runoff Results

Total Rainfall (in) ..... 5.99  
 Total Runoff (in) ..... 5.75  
 Peak Runoff (cfs) ..... 76.90  
 Weighted Curve Number ..... 98.00  
 Time of Concentration (days hh:mm:ss) ..... 0 00:05:00

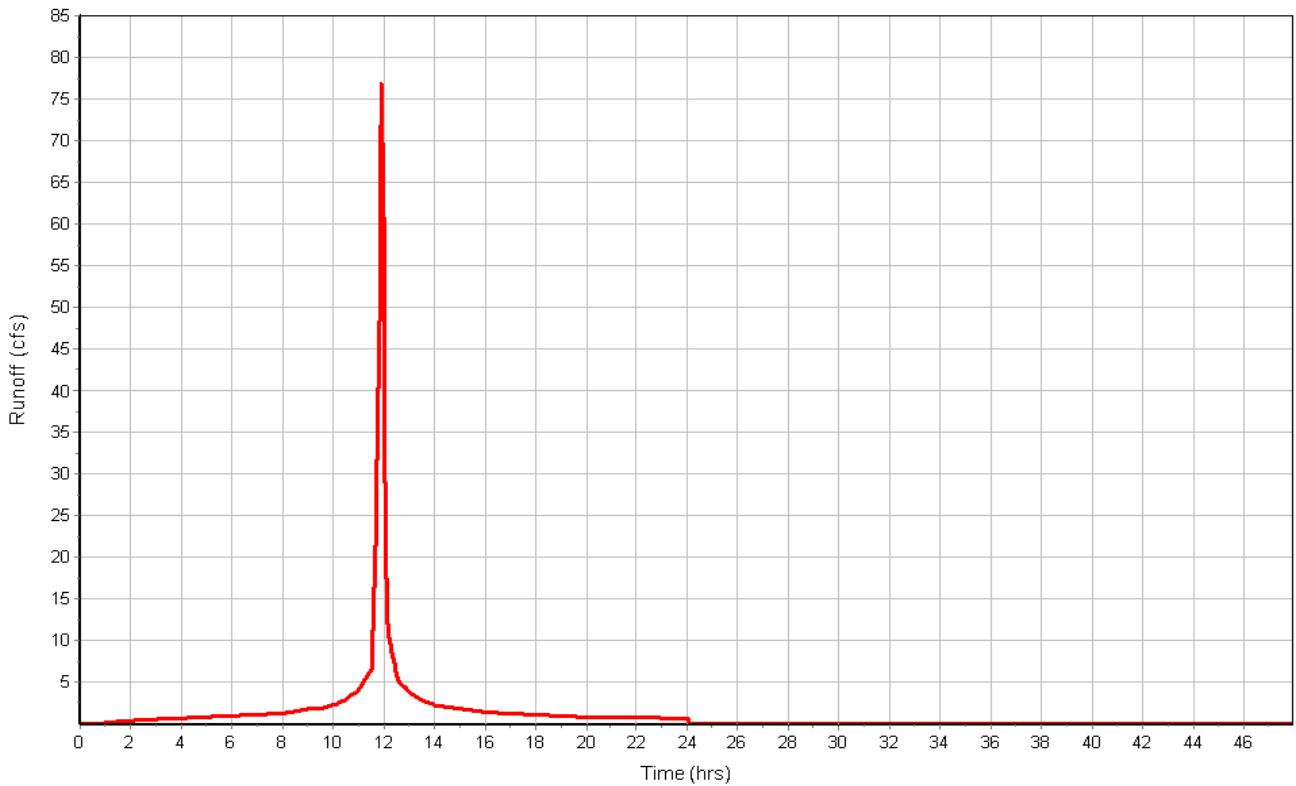


Subbasin : Sub-01

Rainfall Intensity Graph



Runoff Hydrograph



**Subbasin : Sub-02**

**Input Data**

Area (ac) ..... 1.34  
Weighted Curve Number ..... 98.00  
Rain Gage ID ..... Rain Gage-01

**Composite Curve Number**

Soil/Surface Description	Area (acres)	Soil Group	Curve Number
-	1.34	-	98.00
Composite Area & Weighted CN	1.34		98.00

**Time of Concentration**

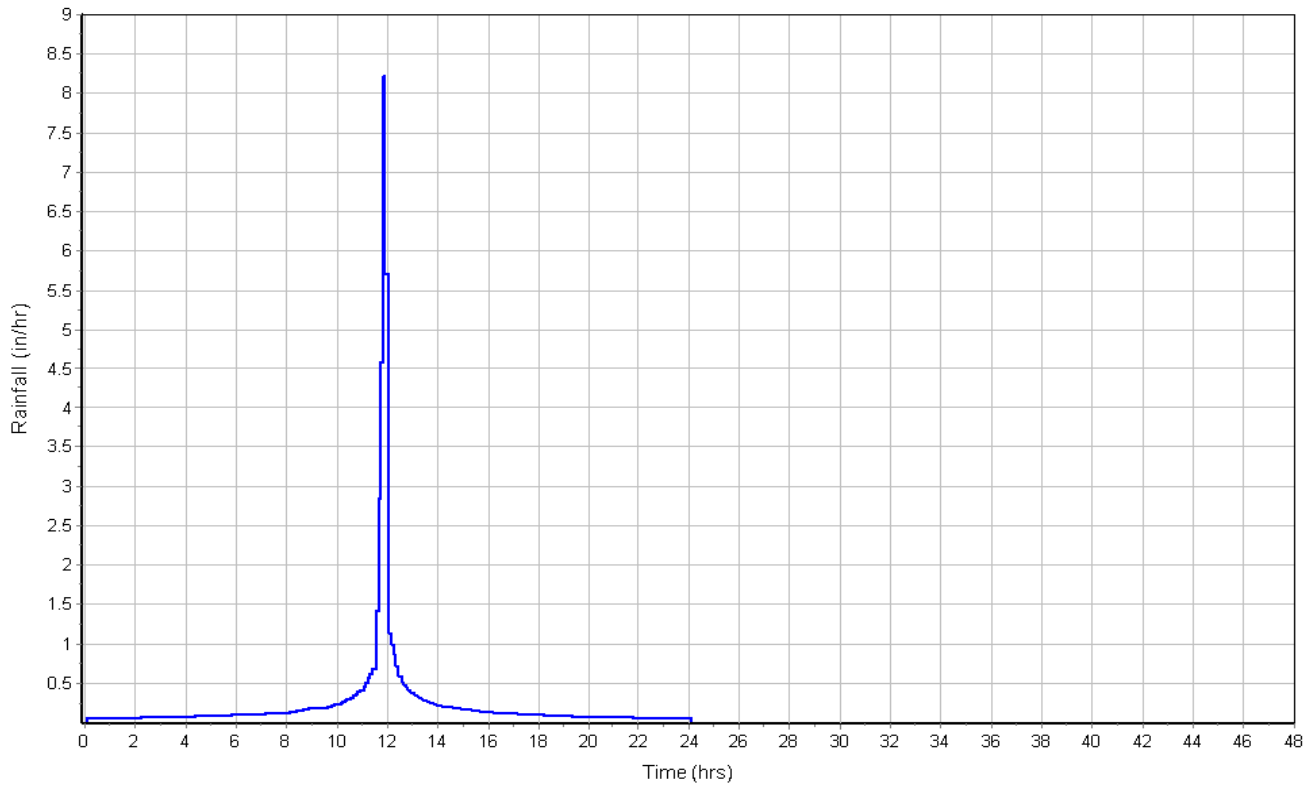
User-Defined TOC override (minutes): 5

**Subbasin Runoff Results**

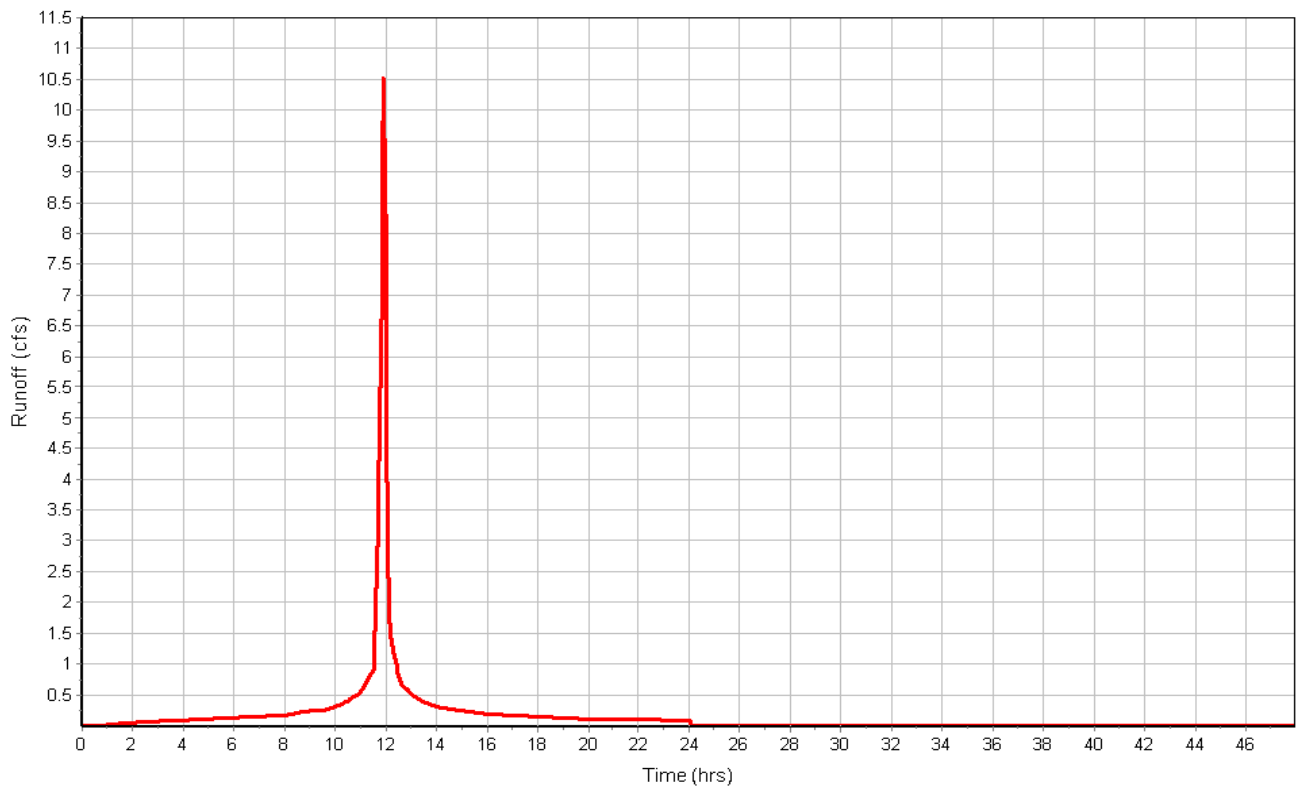
Total Rainfall (in) ..... 5.99  
Total Runoff (in) ..... 5.75  
Peak Runoff (cfs) ..... 10.52  
Weighted Curve Number ..... 98.00  
Time of Concentration (days hh:mm:ss) ..... 0 00:05:00

Subbasin : Sub-02

Rainfall Intensity Graph



Runoff Hydrograph



## Junction Input

SN Element ID	Invert Elevation (ft)	Ground/Rim (Max) Elevation (ft)	Ground/Rim (Max) Offset (ft)	Initial Water Elevation (ft)	Initial Water Depth (ft)	Surcharge Elevation (ft)	Surcharge Depth (ft)	Ponded Area (ft <sup>2</sup> )	Minimum Pipe Cover (ft)
1 Jun-02	596.01	6.00	-590.01	0.00	-596.01	0.00	-6.00	0.00	0.00

## Junction Results

SN Element ID	Peak Inflow	Peak Lateral Inflow	Max HGL Elevation Attained	Max HGL Depth Attained	Max Surcharge Depth Attained	Min Freeboard Attained	Average HGL Elevation Attained	Average HGL Depth Attained	Time of Max HGL Occurrence	Time of Peak Flooding Occurrence	Total Flooded Volume	Total Time Flooded
	(cfs)	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)	(days hh:mm)	(ac-in)	(min)
1 Jun-02	0.00	0.00	596.01	0.00	0.00	3.00	596.01	0.00	0 00:00	0 00:00	0.00	0.00

## Channel Input

SN Element ID	Length (ft)	Inlet Invert Elevation (ft)	Inlet Invert Offset (ft)	Outlet Invert Elevation (ft)	Outlet Invert Offset (ft)	Total Drop (ft)	Average Slope (%)	Shape	Height (ft)	Width (ft)	Manning's Roughness	Entrance Losses	Exit/Bend Losses	Additional Losses	Initial Flap Flow Gate (cfs)
1 PondArea1Channel	1241.00	598.00	3.00	596.01	0.00	1.99	0.1600	Trapezoidal	3.000	15.000	0.0320	0.5000	0.5000	0.0000	0.00 No

## Channel Results

SN Element ID	Peak Flow	Time of Peak Flow Occurrence	Design Flow Capacity	Peak Flow/ Design Flow Ratio	Peak Flow Velocity	Travel Time	Peak Flow Depth	Peak Flow Depth/ Total Depth Ratio	Total Time Surcharged	Froude Number	Reported Condition
	(cfs)	(days hh:mm)	(cfs)		(ft/sec)	(min)	(ft)		(min)		
1 PondArea1Channel	0.00	0 00:00	69.96	0.00	0.00		0.00	0.00	0.00		

## Pipe Input

SN Element ID	Length (ft)	Inlet Invert Elevation (ft)	Inlet Invert Offset (ft)	Outlet Invert Elevation (ft)	Outlet Invert Offset (ft)	Total Drop (ft)	Average Slope (%)	Pipe Shape	Pipe Diameter or Height (ft)	Pipe Width (ft)	Manning's Roughness	Entrance Losses	Exit/Bend Losses	Additional Losses	Initial Flow (cfs)	Flap Gate
1 PondArea1Culvert	40.00	596.01	0.00	595.20	0.00	0.81	2.0200	CIRCULAR	2.000	2.000	0.0250	0.5000	0.5000	0.0000	0.00	No
2 PondArea2Culvert	121.00	590.36	0.36	590.07	0.00	0.29	0.2400	CIRCULAR	2.000	2.000	0.0240	0.5000	1.0000	0.0000	0.00	No



No. of  
Barrels

---

1  
1

## Pipe Results

SN Element ID	Peak Flow	Time of Peak Flow Occurrence	Design Flow Capacity	Peak Flow/ Design Flow Ratio	Peak Flow Velocity	Travel Time	Peak Flow Depth	Peak Flow Depth/ Total Depth Ratio	Total Time Surcharged	Froude Number	Reported Condition
	(cfs)	(days hh:mm)	(cfs)		(ft/sec)	(min)	(ft)		(min)		
1 PondArea1Culvert	0.00	0 00:00	16.74	0.00	0.00		0.00	0.00	0.00		Calculated
2 PondArea2Culvert	9.30	0 12:20	6.00	1.55	3.57	0.56	1.54	0.77	0.00		> CAPACITY

# Storage Nodes

## Storage Node : PondArea1

### Input Data

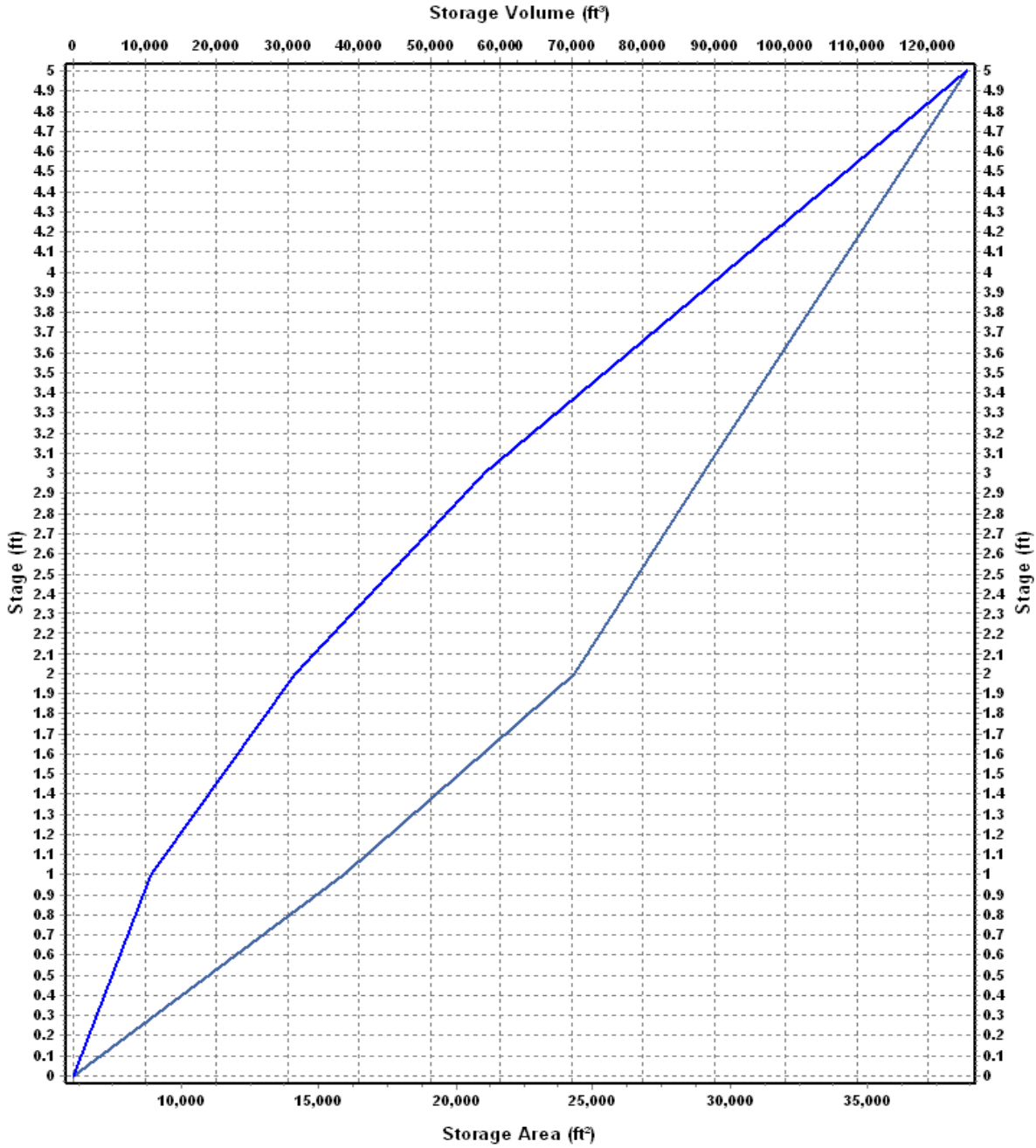
Invert Elevation (ft) ..... 595.00  
Max (Rim) Elevation (ft) ..... 598.96  
Max (Rim) Offset (ft) ..... 3.96  
Initial Water Elevation (ft) ..... 595.00  
Initial Water Depth (ft) ..... 0.00  
Ponded Area (ft<sup>2</sup>) ..... 0.00  
Evaporation Loss ..... 0.00

### Storage Area Volume Curves

Storage Curve : Storage-01

Stage	Storage Area	Storage Volume
(ft)	(ft <sup>2</sup> )	(ft <sup>3</sup> )
0	6061.76	0.000
1	15942.88	11002.32
2	24307.18	31127.35
3	29017.09	57789.49
5	38618.549	125425.13

### Storage Area Volume Curves



— Storage Area    — Storage Volume

## Storage Node : PondArea1 (continued)

### Output Summary Results

Peak Inflow (cfs) .....	10.52
Peak Lateral Inflow (cfs) .....	10.52
Peak Outflow (cfs) .....	0.00
Peak Exfiltration Flow Rate (cfm) .....	0.00
Max HGL Elevation Attained (ft) .....	596.86
Max HGL Depth Attained (ft) .....	1.86
Average HGL Elevation Attained (ft) .....	596.40
Average HGL Depth Attained (ft) .....	1.4
Time of Max HGL Occurrence (days hh:mm) .....	1 00:20
Total Exfiltration Volume (1000-ft <sup>3</sup> ) .....	0.000
Total Flooded Volume (ac-in) .....	0
Total Time Flooded (min) .....	0
Total Retention Time (sec) .....	0.00

## Storage Node : PondArea2

### Input Data

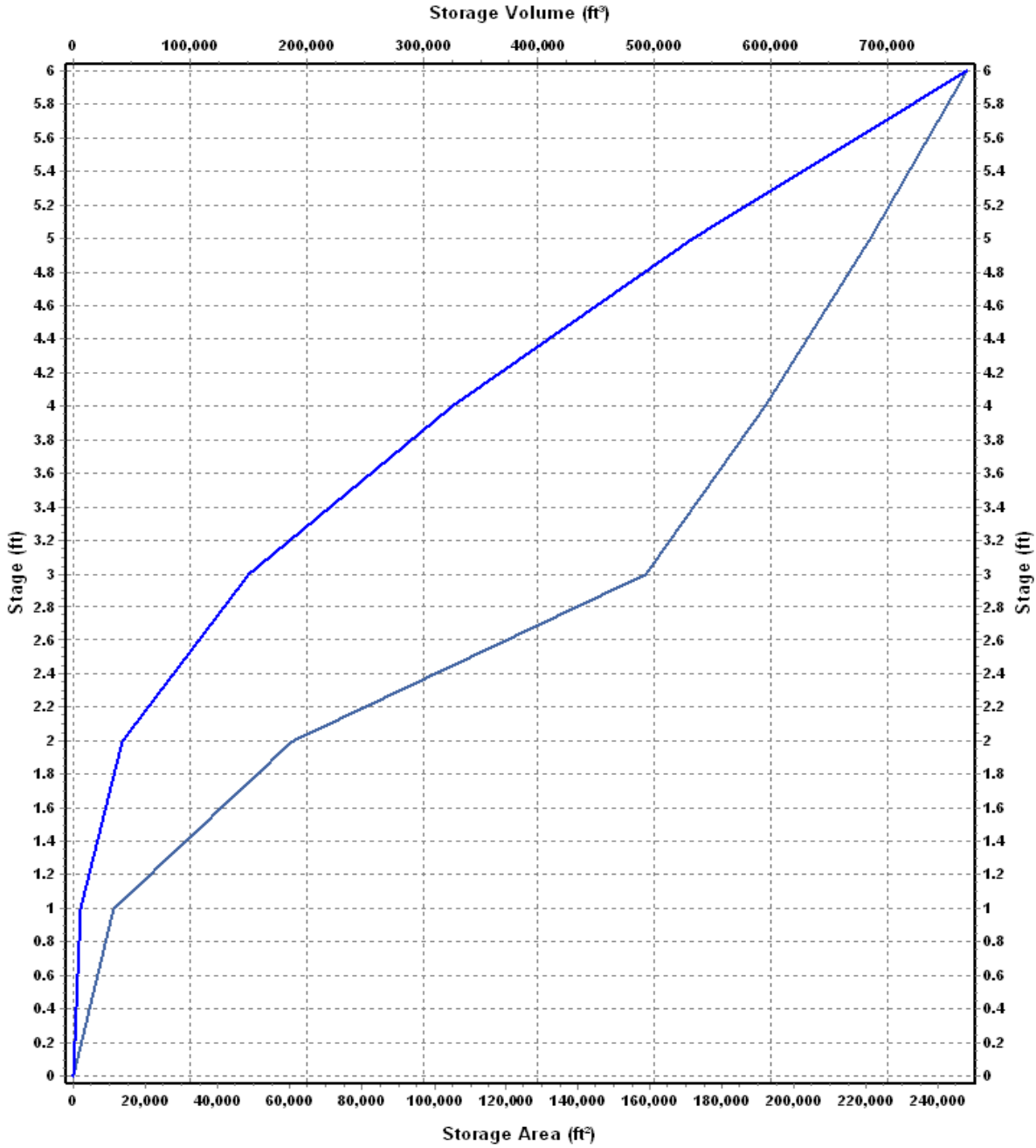
Invert Elevation (ft) ..... 590.00  
Max (Rim) Elevation (ft) ..... 596.68  
Max (Rim) Offset (ft) ..... 6.68  
Initial Water Elevation (ft) ..... 590.36  
Initial Water Depth (ft) ..... 0.36  
Ponded Area (ft<sup>2</sup>) ..... 0.00  
Evaporation Loss ..... 0.00

### Storage Area Volume Curves

Storage Curve : Storage-02

Stage	Storage Area	Storage Volume
(ft)	(ft <sup>2</sup> )	(ft <sup>3</sup> )
0	0	0.000
1	11213.61	5606.81
2	60746.13	41586.68
3	158834.96	151377.23
4	191913.30	326751.36
5	221215.98	533316.00
6	247890.20	767869.09

### Storage Area Volume Curves



— Storage Area    — Storage Volume

## Storage Node : PondArea2 (continued)

### Output Summary Results

Peak Inflow (cfs) .....	76.88
Peak Lateral Inflow (cfs) .....	76.88
Peak Outflow (cfs) .....	9.30
Peak Exfiltration Flow Rate (cfm) .....	0.00
Max HGL Elevation Attained (ft) .....	592.53
Max HGL Depth Attained (ft) .....	2.53
Average HGL Elevation Attained (ft) .....	591.10
Average HGL Depth Attained (ft) .....	1.1
Time of Max HGL Occurrence (days hh:mm) .....	0 12:20
Total Exfiltration Volume (1000-ft <sup>3</sup> ) .....	0.000
Total Flooded Volume (ac-in) .....	0
Total Time Flooded (min) .....	0
Total Retention Time (sec) .....	0.00



Established in 1960, Golder Associates is a global, employee-owned organization that helps clients find sustainable solutions to the challenges of finite resources, energy and water supply and management, waste management, urbanization, and climate change. We provide a wide range of independent consulting, design, and construction services in our specialist areas of earth, environment, and energy. By building strong relationships and meeting the needs of clients, our people have created one of the most trusted professional services organizations in the world.

Africa	+ 27 11 254 4800
Asia	+ 852 2562 3658
Australasia	+ 61 3 8862 3500
Europe	+ 356 21 42 30 20
North America	+ 1 800 275 3281
South America	+ 56 2 2616 2000

[solutions@golder.com](mailto:solutions@golder.com)  
[www.golder.com](http://www.golder.com)

**Golder Associates Inc.**  
**15851 South U.S. 27, Suite 50**  
**Lansing, MI 48906 USA**  
**Tel: (517) 482-2262**  
**Fax: (517) 482-2460**



**Engineering Earth's Development, Preserving Earth's Integrity**

Golder, Golder Associates and the GA globe design are trademarks of Golder Associates Corporation